Amendments to the Specification:

Please replace the paragraph beginning at page 2, line 9 with the following amended paragraph.

FIG. 1 shows a typical prior art ballast circuit 10 having a conventional output isolation transformer 12. A rectifier/filter 14 receives an AC input signal on first and second input terminals 16a,b and provides positive and negative voltage rails 18,20. Inductively coupled inductors L1-A, L1-B can be provided on the respective positive and negative rails 18, 20. First and second switching elements 22,24 are coupled across the rails in a well known half-bridge configuration. A primary winding 26, e.g., 1.5 mH 50 turns, of the output isolation transformer combines with a resonating capacitor 28 to form a parallel resonating circuit. A secondary winding 30, e.g., 100 turns, of the transformer energizes first and second lamps LP1, LP2 each of which is coupled in ~~parallel~~ series with respective lamp capacitors CL1, CL2. In this well known configuration, the secondary winding 30 of the transformer isolates the lamp terminals from the resonating circuit so as to limit the ground fault current flow. In the event a technician inadvertently touches a lamp terminal and thereby provides a current path to ground, the current flow through the technician's body is limited to a safe level to prevent injury. Underwriter's Laboratories promulgates standards for acceptable ballast ground fault current levels.

Please replace the paragraph beginning at page 9, line 4 with the following amended paragraph.

In general, the turn ratios of the first and second secondary windings ~~L2-A, L2-B~~ L2-B, L2-C and the primary winding L2-A can be selected to budget the lamp strike voltage as desired since the winding voltages are additively applied across the lamps. Thus, the output isolation transformer circuit of the present invention provides the flexibility to control the voltages generated on the windings. For example, a combined potential of 750 VRMS can be generated on the primary and secondary windings to strike an eight foot lamp. The 750 VRMS can be safely generated by dividing the voltage between the primary and secondary windings with respect to AC ground. It is understood that the strike voltage can be apportioned among the windings as desired. In addition, the 750 VRMS can be provided by the transformer with minimal corona effects in comparison to the prior art circuit shown in FIG. 1.

Please replace the paragraph beginning at page 10, line 16 with the following amended paragraph.

FIG. 4 shows an exemplary resonant circuit 201 having power feedback in accordance with the present invention. A multi-bridge rectifier 201 includes pairs (DF11, DF12), (DF21, DF22), ...(DFN1, DFN2) of rectifying diodes coupled end-to end. A top 202 of the multi-bridge rectifier ~~200~~ 201 is coupled to a bottom ~~202~~ 203 of a low frequency input rectifier 204 and a bottom 206 of the multi-bridge rectifier is coupled to a negative rail 208 of the inverter. A top of the input rectifier 210 is coupled to the positive rail 212 of the inverter.